# Designer's™ Data Sheet TMOS E-FET™ **Power Field Effect Transistor N–Channel Enhancement–Mode Silicon Gate**

This advanced TMOS power FET is designed to withstand high energy in the avalanche and commutation modes. This new energy efficient design also offers a drain–to–source diode with fast recovery time. Designed for high voltage, high speed switching applications in power supplies, converters, PWM motor controls, and other inductive loads. The avalanche energy capability is specified to eliminate the guesswork in designs where inductive loads are switched and offer additional safety margin against unexpected voltage transients.



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# MTY30N50E

**Motorola Preferred Device**

**TMOS POWER FET 30 AMPERES 500 VOLTS RDS(on) = 0.15 OHM**



**CASE 340G–02, STYLE 1 TO–264**



**MAXIMUM RATINGS** ( $T_C = 25^\circ \text{C}$  unless of

• Diode is Characterized for Use in Bridge Circuits • IDSS and VDS(on) Specified at Elevated Temperature

• Avalanche Energy Specified



**Designer's Data for "Worst Case" Conditions** — The Designer's Data Sheet permits the design of most circuits entirely from the information presented. SOA Limit curves — representing boundaries on device characteristics — are given to facilitate "worst case" design.

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**Preferred** devices are Motorola recommended choices for future use and best overall value.



**REV 2**

**ELECTRICAL CHARACTERISTICS** (T<sub>J</sub> = 25°C unless otherwise noted)



(1) Pulse Test: Pulse Width  $\leq$  300  $\mu$ s, Duty Cycle  $\leq$  2%.

(2) Switching characteristics are independent of operating junction temperature.

# **TYPICAL ELECTRICAL CHARACTERISTICS**







**Figure 2. Transfer Characteristics**



**Figure 3. On–Resistance versus Drain Current and Temperature**



**Figure 5. On–Resistance Variation with Temperature**



**Figure 4. On–Resistance versus Drain Current and Gate Voltage**



**Figure 6. Drain–To–Source Leakage Current versus Voltage**

## **POWER MOSFET SWITCHING**

Switching behavior is most easily modeled and predicted by recognizing that the power MOSFET is charge controlled. The lengths of various switching intervals (∆t) are determined by how fast the FET input capacitance can be charged by current from the generator.

The published capacitance data is difficult to use for calculating rise and fall because drain–gate capacitance varies greatly with applied voltage. Accordingly, gate charge data is used. In most cases, a satisfactory estimate of average input current  $(I_G(A_V))$  can be made from a rudimentary analysis of the drive circuit so that

 $t = Q/I$  $(AV)$ 

During the rise and fall time interval when switching a resistive load, V<sub>GS</sub> remains virtually constant at a level known as the plateau voltage, VSGP. Therefore, rise and fall times may be approximated by the following:

$$
t_{\rm r} = Q_2 \times R_G/(V_{GG} - V_{GSP})
$$

 $t_f = Q_2 \times R_G/V_GSP$ 

where

24000

20000

16000

12000

Crss

C, CAPACITANCE (pF)

C, CAPACITANCE (pF)

8000

4000

0

 $V_{GG}$  = the gate drive voltage, which varies from zero to  $V_{GG}$ 

 $R_G$  = the gate drive resistance

and Q2 and VGSP are read from the gate charge curve.

During the turn–on and turn–off delay times, gate current is not constant. The simplest calculation uses appropriate values from the capacitance curves in a standard equation for voltage change in an RC network. The equations are:

**Figure 7a. Capacitance Variation**

 $td(on) = RG C$ iss  $In [VGG/(VGG - VGSP)]$  $t_{\rm d(off)}$  = R<sub>G</sub> C<sub>iss</sub> In (V<sub>GG</sub>/V<sub>GSP</sub>)

 $\leftarrow$   $V_{GS}$   $\leftarrow$   $V_{DS}$ 

Crss

The capacitance  $(C<sub>iss</sub>)$  is read from the capacitance curve at a voltage corresponding to the off–state condition when calculating  $t_{d(0n)}$  and is read at a voltage corresponding to the on–state when calculating  $t_{\text{d(off)}}$ .

At high switching speeds, parasitic circuit elements complicate the analysis. The inductance of the MOSFET source lead, inside the package and in the circuit wiring which is common to both the drain and gate current paths, produces a voltage at the source which reduces the gate drive current. The voltage is determined by Ldi/dt, but since di/dt is a function of drain current, the mathematical solution is complex. The MOSFET output capacitance also complicates the mathematics. And finally, MOSFETs have finite internal gate resistance which effectively adds to the resistance of the driving source, but the internal resistance is difficult to measure and, consequently, is not specified.

The resistive switching time variation versus gate resistance (Figure 9) shows how typical switching performance is affected by the parasitic circuit elements. If the parasitics were not present, the slope of the curves would maintain a value of unity regardless of the switching speed. The circuit used to obtain the data is constructed to minimize common inductance in the drain and gate circuit loops and is believed readily achievable with board mounted components. Most power electronic loads are inductive; the data in the figure is taken with a resistive load, which approximates an optimally snubbed inductive load. Power MOSFETs may be safely operated into an inductive load; however, snubbing reduces switching losses.



**Variation**



**Figure 8. Gate Charge versus Gate–to–Source Voltage**

**Figure 9. Resistive Switching Time Variation versus Gate Resistance**

#### **DRAIN–TO–SOURCE DIODE CHARACTERISTICS**



**Figure 10. Diode Forward Voltage versus Current**

#### **SAFE OPERATING AREA**

The Forward Biased Safe Operating Area curves define the maximum simultaneous drain–to–source voltage and drain current that a transistor can handle safely when it is forward biased. Curves are based upon maximum peak junction temperature and a case temperature (TC) of 25°C. Peak repetitive pulsed power limits are determined by using the thermal response data in conjunction with the procedures discussed in AN569, "Transient Thermal Resistance–General Data and Its Use."

Switching between the off–state and the on–state may traverse any load line provided neither rated peak current (IDM) nor rated voltage (V<sub>DSS</sub>) is exceeded and the transition time  $(t_r,t_f)$  do not exceed 10  $\mu$ s. In addition the total power averaged over a complete switching cycle must not exceed  $(TJ(MAX) - TC)/(R_{\theta JC}).$ 

A Power MOSFET designated E–FET can be safely used in switching circuits with unclamped inductive loads. For reliable operation, the stored energy from circuit inductance dissipated in the transistor while in avalanche must be less than the rated limit and adjusted for operating conditions differing from those specified. Although industry practice is to rate in terms of energy, avalanche energy capability is not a constant. The energy rating decreases non–linearly with an increase of peak current in avalanche and peak junction temperature.

Although many E–FETs can withstand the stress of drain– to–source avalanche at currents up to rated pulsed current (IDM), the energy rating is specified at rated continuous current  $(I_D)$ , in accordance with industry custom. The energy rating must be derated for temperature as shown in the accompanying graph (Figure 12). Maximum energy at currents below rated continuous I<sub>D</sub> can safely be assumed to equal the values indicated.

# **SAFE OPERATING AREA**





**Figure 13. Thermal Response**



**Figure 14. Diode Reverse Recovery Waveform**

# **PACKAGE DIMENSIONS**



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